



**APPLICATION FOR UNITED STATES
LETTERS PATENT**

**ULTRASONIC CONTRAST AGENT IMAGING BY DUALBAND PULSE
TRANSMISSION**

Inventor(s):

**Rune HANSEN
Bjørn A.J. ANGELSEN**

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TRANSMISSION**

CROSS REFERENCE TO RELATED APPLICATION

[0001] This application discloses and claims priority from U.S. Provisional Patent Application Serial No. 60/449,222, filed on February 20, 2003.

BACKGROUND OF THE INVENTION

1. Field of the Invention

[0002] This invention relates to methods and systems for ultrasonic detection and imaging of contrast agents located in soft tissue or tissue fluids.

2. Description of the Related Art

[0003] Ultrasound contrast agents are typically made as solutions of micro gas bubbles or nano lipid particles. The gas bubbles typically show strong and nonlinear scattering of the ultrasound, a phenomenon that is used to differentiate the contrast agent signal from the tissue signal. In the earliest applications (~1985) the increased scattering from the contrast agent within the transmitted frequency band was used to enhance the scattering from blood. Later, second harmonic components in the nonlinearly scattered signal were used to further enhance the contrast agent signal above the tissue signal in methods generally referred to as nonlinear contrast harmonic imaging.

[0004] The following two signal power ratios have vital importance for the quality of performance of a contrast imaging system:

[0005] CTR-- Contrast signal to Tissue signal Ratio. This gives the ratio of the signal power scattered from the contrast agent in a region to the signal power scattered from the tissue in that region. This ratio is often referred to as specificity.

[0006] CNR-- Contrast signal to Noise Ratio. This gives the ratio of the signal power scattered from the contrast agent in a region to the noise power in that region. This ratio is often referred to as sensitivity.

[0007] The CNR determines the maximum depth for imaging the contrast agent while the CTR describes the enhancement of the contrast agent signal above the tissue signal in the image and thus the capability of differentiating contrast signal from tissue signal. High values of both these ratios are therefore necessary for good imaging of the contrast agent.

[0008] The nonlinear distortion of the signal scattered from the contrast agent is much stronger than for the tissue signal, a phenomenon that is extensively used to enhance the CTR. In one method, received tissue signal components in the transmitted frequency band (linear components) are reduced by combining the received signal from two transmitted pulses with different amplitudes. In other methods, the second harmonic band of the nonlinearly scattered signal is obtained either by bandpass filtering or by combining the received signals from two or more transmitted pulses with different polarities.

[0009] Wave propagation in soft tissue is a weak nonlinear process for intensities common in medical ultrasound imaging. The local nonlinearity is low and the distortion of the wave accumulates gradually in the propagation direction of the wave. Wave propagation in a homogeneous medium with acoustic absorption may be mathematically described by the following equation

$$\nabla^2 p - \frac{1}{c^2} \frac{\partial^2 p}{\partial t^2} - \frac{1}{c^2} h \otimes \frac{\partial^2 p}{\partial t^2} = -\kappa\beta \frac{1}{c^2} \frac{\partial^2 p^2}{\partial t^2} \quad (1)$$

where p is the acoustic pressure, c is the speed of sound, ∇^2 is the Laplacian sum of the second derivatives with respect to the three Cartesian coordinates, h is a causal filter, κ is the compressibility, β is a nonlinearity parameter for the propagation medium, and t is time. The integral term is responsible for acoustic absorption while the term on the right-hand side is responsible for nonlinear effects in the wave propagation.

[0010] In medical ultrasound imaging, a good approximation of the transmitted field is often to first calculate the linear transmitted field by discarding the term on the right-hand side in the above equation and to use this linear field as a source for the second harmonic component which then is calculated by using the full equation. This is usually referred to as the quasi-linear approximation of the nonlinear wave equation and the nonlinear component is then produced by a quadratic effect of the linear transmitted field only.

[0011] This is a first approximation of the nonlinearity of the propagation medium but since wave propagation in absorbing soft tissue at intensities common in medical ultrasound imaging is a relatively weak nonlinear process, this approximation is good.

[0012] From a homogeneous medium described by this equation there will be no back-scattered waves. In an actual medical ultrasound imaging situation, tissue heterogeneities are responsible for producing the back-scattered waves and hence the image displayed on the ultrasound scanner. In numerical computer simulations, a simulated scatterer can be inserted at a desired location in the calculated transmit field

to produce a back-scattered wave. The scattering process can then, as in the case of the heterogeneous tissue, usually be modeled as a linear process. In the case of the point scatterer, the scattered amplitude is proportional to the square of the frequency.

[0013] Ultrasound contrast agents, and in particular gas filled bubbles, generally exhibit a strong nonlinear scattering when subject to an imaging ultrasound pulse, and higher order nonlinear terms are not negligible. A well known nonlinear equation for the motion of the fluid around a spherical pulsating gas bubble is the Rayleigh-Plesset equation. The radius oscillation of the bubble is then expressed as

$$\rho(a\ddot{a} + \frac{3}{2}\dot{a}^2) = p(a,t) - p_0 - p_i(t) \quad (2)$$

where a is the radius, \dot{a} and \ddot{a} is the velocity and acceleration of the bubble radius, ρ is the density of the surrounding fluid, p_0 is the ambient equilibrium pressure, $p_i(t)$ is the driving pressure, and $p(a,t)$ is the pressure at the bubble surface. Nonlinear effects of the gas and encapsulating thin shell, surface tension, and viscosity may be incorporated in the first term on the right-hand side of Eq.2.

SUMMARY OF THE INVENTION

[0014] To increase the nonlinear fundamental and/or second and/or third and/or fourth harmonic CNR, pulses with frequency components in two frequency bands, in particular a fundamental band and its second harmonic band, are transmitted. With stationary tissue, resulting linear and first order nonlinear harmonic tissue components can be significantly reduced or canceled by a pulse inversion technique, where for example two multiband pulses with opposite polarities on the second harmonic band are consecutively transmitted and the received signals from these two pulses are combined through summation or subtraction. With nonstationary tissue, more than two transmit pulses may be used to account for the tissue movement between each pulse.

[0015] Other objects and features of the present invention will become apparent from the following detailed description considered in conjunction with the accompanying drawings. It is to be understood, however, that the drawings are designed solely for purposes of illustration and not as a definition of the limits of the invention, for which reference should be made to the appended claims. It should be further understood that the drawings are not necessarily drawn to scale and that, unless otherwise indicated, they are merely intended to conceptually illustrate the structures and procedures described herein.

BRIEF DESCRIPTION OF THE DRAWINGS

In the drawings:

[0016] The decibel plots of scattered pressure from a contrast bubble and transmit pressure pulses should not be compared in terms of absolute levels of harmonic components. It is the relative levels of harmonic components which is visualized in these figures.

[0017] **FIG.1** shows an example of a fundamental (solid line) and second harmonic (dashed line) pulse. In the upper panel, the phase angle of the second harmonic component relative to the fundamental components is 0 while in the lower panel, this phase angle is set to $\pi/2$.

[0018] **FIG.2** illustrates four possible dual frequency band pulse designs using a relative phase angle of 0 and $\pi/2$ in the upper and lower panels, respectively.

[0019] **FIG.3** shows the spectrum of the pulses in **FIG.2**.

[0020] **FIG.4** depicts the spectrum of the resulting transmit pulse at 6 cm on the symmetry axis of an annular transducer of radius 1 cm and focus at 12 cm when driven by pulse 103 in **FIG.2**.

[0021] **FIG.5** shows the spectrum of the resulting pulse summation transmit signal at 6 cm on the symmetry axis obtained using the drive pulses 103 and 104 in **FIG.2** to drive the annular transducer.

[0022] **FIG.6** shows the spectrum of the resulting pulse subtraction transmit signal at 6 cm on the symmetry axis obtained using the drive pulses 103 and 104 in **FIG.2** to drive the transducer.

[0023] FIG.7 depicts transmit field at 6 cm on the symmetry axis obtained using the fundamental frequency band only in FIG.3 to drive the annular transducer.

[0024] FIG.8 displays the spectrum of a scattered bubble signal obtained with the transmit field at 6 cm on the symmetry axis using the fundamental frequency band only in FIG.3 to drive the annular transducer.

[0025] FIG.9 depicts the spectrum of a scattered bubble signal obtained with the transmit field at 6 cm on the symmetry axis using pulse 104 in FIG.2 to drive the annular transducer.

[0026] FIG.10 depicts the spectrum of a scattered bubble signal obtained with the transmit field at 6 cm on the symmetry axis using pulse 103 in FIG.2 to drive the annular transducer.

[0027] FIG.11. shows the spectrum of the resulting pulse summation bubble signal at 6 cm on the symmetry axis obtained using the drive pulses 101 and 102 in FIG.2 on the transducer.

[0028] FIG.12 shows the spectrum of the resulting pulse subtraction bubble signal at 6 cm on the symmetry axis obtained using the drive pulses 103 and 104 in FIG.2 on the transducer.

[0029] FIG.13 displays the resulting transmit pulse in the time domain at 10 cm on the symmetry axis using pulse 102 in FIG.2 on the annular transducer.

[0030] FIG.14 displays the resulting transmit pulse in the time domain at 10 cm on the symmetry axis using pulse 101 in FIG.2 on the annular transducer.

[0031] FIG.15 displays the spectrum of the resulting transmit pulse at 10 cm on the symmetry axis using pulse 101 in FIG.2 on the annular transducer.

[0032] FIG.16 shows the spectrum of the resulting pulse summation transmit signal at 10 cm on the symmetry axis obtained using the drive pulses 101 and 102 in FIG.2 on the transducer.

[0033] FIG.17 shows the spectrum of the resulting pulse subtraction transmit signal at 10 cm on the symmetry axis obtained using the drive pulses 101 and 102 in FIG.2 on the transducer.

[0034] FIG.18 depicts the spectrum of a scattered bubble signal obtained with the transmit field at 10 cm on the symmetry axis using the fundamental frequency band only in FIG.3 to drive the annular transducer.

[0035] FIG.19 depicts the spectrum of a scattered bubble signal obtained with the transmit field at 10 cm on the symmetry axis using pulse 101 in FIG.2 to drive the annular transducer.

[0036] FIG.20 shows the spectrum of the resulting pulse subtraction bubble signal at 10 cm on the symmetry axis obtained using the drive pulses 101 and 102 in FIG.2 on the transducer.

DETAILED DESCRIPTION OF THE PRESENTLY PREFERRED EMBODIMENTS

[0037] A first aspect of the present invention is performed by transmitting a pulse containing two frequency bands, in particular a fundamental band and its second harmonic band where the relative phase relations between the two transmitted frequency bands are adjustable, into an area containing contrast agent. If the intensity of the transmitted pulse is relatively low, the propagation medium without contrast agent will behave approximately linearly while the contrast agent will behave strongly nonlinearly. The area containing contrast agent will thus scatter frequency components not transmitted, in particular third and fourth harmonic components, which can be used for image reconstruction of the area of interest. By using a dual frequency band pulse with adjustable relative phase angle between the two transmitted frequency bands, a large flexibility with respect to transmit pulse design is allowed.

[0038] If the transmit fundamental frequency band is chosen such that the resulting third or fourth harmonic component is in the vicinity of the contrast bubble resonance frequency, the bubble will respond with strong third and/or fourth harmonic components when driven by the low intensity dual frequency band pulse. Properly selecting the relative phase angle between the transmitted fundamental and second harmonic band one is able to manipulate and optimize the third and/or fourth harmonic bubble response.

[0039] In a second aspect of the present invention, a pulse similar to the one in the first aspect is transmitted, scattered, received, and stored. Then a second pulse is transmitted down the same line of sight where the polarity of the second harmonic

frequency band is inverted relative to the first transmitted pulse and a general form of pulse inversion is performed on the resulting received signals. The two transmitted pulses may for example be expressed as

$$p_1(t) = a_1(t) \sin(\omega t) + a_2(t) \sin(2\omega t - \varphi_1) \quad (3)$$

$$p_2(t) = a_3(t) \sin(\omega t) - a_4(t) \sin(2\omega t - \varphi_2) \quad (4)$$

where $a_n(t)$ are positive amplitude functions, ω is the angular frequency, and φ_n are arbitrary phase angles. These phase angles are in the present invention given as a fraction of the temporal period of the second harmonic component. We define the indicated phase angle to zero when the zero-crossings of the fundamental pressure component coincide with every second zero-crossing of the second harmonic pressure component. In the present invention, this phase angle will typically be between 0 and $\pi/2$. The fact that a_3 may be different from a_1 and a_4 may be different from a_2 gives the flexibility to further utilize the assumption of strong versus weak nonlinearity of a propagation medium containing and not containing contrast agent, respectively.

[0040] If $a_3 = a_1$, $a_4 = a_2$, and $\varphi_2 = \varphi_1$ in Eqs.3 and 4, performing pulse summation on two resulting received signals, s_1 and s_2 , from a region of tissue not containing contrast agents so that the nonlinearity is well described by the quasi-linear approximation, gives

$$s_1(t) + s_2(t) = L(2a_1(t) \sin(\omega t) + 2a_1^2(t) \sin^2(\omega t) + 2a_2^2(t) \sin^2(2\omega t - \varphi_1)) \quad (5)$$

where L is a linear operator. The first term on the right-hand side is the linear component in the summed signal. The linear component of the transmitted second harmonic component is canceled in the pulse inversion technique due to the phase inversion in Eqs.3 and 4. In the two last terms on the right-hand side in Eq.5 we have the first order nonlinear components in the summed signal. These nonlinear terms consist of a second harmonic component from the transmitted fundamental component, and a second harmonic component from the transmitted second harmonic component (i.e. a fourth harmonic component relative to the transmitted fundamental band). The nonlinear sum and difference frequencies producing third and fundamental harmonic components have hence been canceled in the pulse inversion process for a propagation medium of weak nonlinearity described by the quasi-linear approximation.

[0041] If we instead subtract the two received signals, s_1 and s_2 , from a region of tissue not containing contrast agents, and where nonlinearities hence are assumed to be described by the quasi-linear approximation, we obtain

$$s_1(t) - s_2(t) = L(2a_2(t)\sin(2\omega t - \varphi_1) + 4a_1(t)a_2(t)\sin(\omega t)\sin(2\omega t - \varphi_1)) \quad (6)$$

[0042] Now, the linear transmitted fundamental band is canceled in the pulse inversion process while the linear transmitted second harmonic band is doubled. The first order nonlinear term, second term on the right-hand side in Eq.6, now consists of a nonlinear mixing term between the linear transmitted fundamental band and the second harmonic band producing nonlinear fundamental and third harmonic components.

Performing a subtraction instead of a summation of the received scattered signals hence cancels the first order nonlinear fourth harmonic components from the tissue.

[0043] Nonlinear scattering from contrast bubbles will not be adequately described by the quasi-linear approximation. Third and fourth harmonic bubble signals will thus not be significantly reduced when performing the indicated pulse summation and pulse subtraction process, respectively. Also, a very strong nonlinear fundamental contrast component can be obtained with the pulse subtraction technique.

[0044] In a third aspect of the invention a sequence of pulses as in the second aspect is transmitted down each line of sight. Every second transmitted pulse has inverted polarity on its second harmonic band relative to the previous one as explained above. Only a couple of the transmitted pulses may be used for image reconstruction which is done performing a general form of pulse inversion or applying standard Doppler processing techniques. Transmitting a sequence of pulses like this instead of only two pulses may be advantageous in relation to moving tissue problems encountered in pulse inversion contrast techniques.

[0045] In the second and third aspect of the present invention, two or more pulses are to be transmitted down each line of sight, i.e. in one beam direction. If the image is formed by stepping the beam direction, for example as with electronic scanning, the beam direction can be the same for as long as necessary and several consecutive pulses can be transmitted down the same line of sight.

[0046] The image may also be formed using a beam that is continuously swept with a mechanical motion of the transducer. It is then important that this sweeping

motion is slow in relation to the pulse transmit rate so that the received signals from the transmitted pulses being combined to detect the contrast agent signal originate from substantially the same region in the tissue.

[0047] The subsequent received signals can be combined through simple summation or subtraction, or the received signals may be linearly combined.

[0048] **FIG.1** shows an example of a fundamental (solid line) and second harmonic (dashed line) pulse. In the upper panel, the phase angle of the second harmonic component relative to the fundamental components is 0 while in the lower panel, this phase angle is set to $\pi/2$.

[0049] As already indicated, transmitting dual frequency band pulses with adjustable relative phase relations (selecting φ) gives a large flexibility with respect to transmit pulse design. The pulses **101**, **102**, **103**, and **104** depicted in **FIG.2** show examples of four possible transmit pulse designs. Pulse **101** is described by Eq.3 where $a_2 = 0.8a_1$ and $\varphi_1 = 0$ while pulse **102** is described by Eq.4 where $a_3 = a_1$, $a_4 = a_2$, and $\varphi_2 = \varphi_1$. Similarly, pulse **103** is described by Eq.3 where $a_2 = 0.8a_1$ and $\varphi_1 = \pi/2$ while pulse **104** is described by Eq.4 where $a_3 = a_1$, $a_4 = a_2$, and $\varphi_2 = \varphi_1$. Comparing pulse **101** and **102** there is a small difference in terms of maximum amplitude levels due to the phase inversion of the second harmonic band whereas in pulse **103** and **104** there is a major asymmetry in terms of positive and negative amplitude levels.

[0050] The absolute value of the Fourier Transform will be the same for the four pulses in **FIG.2** and is shown in **FIG.3**. We see that the pulses contain a fundamental 1 MHz component (**211**) and a second harmonic 2 MHz component (**212**).

[0051] The pulses in **FIG.2** are then used as excitation pulses on an annular transducer with radius equal to 1 cm and a geometrical focus at 12 cm. A numerical simulation program developed in our group is then used to calculate the transmitted acoustical fields from this annular transducer when driven by the excitation pulses consisting of both a fundamental band (**211**) and a second harmonic band (**212**). The simulation program includes effects of diffraction, frequency dependent absorption, and nonlinear tissue elasticity. Effects of nonlinear tissue elasticity are not limited by the quasi-linear approximation in the simulation program.

[0052] **FIG.4** shows the spectrum of the transmit field at 6 cm on the symmetry axis when pulse **103** is applied on the annular transducer. There is a strong linear fundamental (**361**) and linear second harmonic (**362**) band and weaker nonlinear third (**363**) and fourth (**364**) harmonic bands introduced due to nonlinear tissue elasticity.

[0053] We may now perform a pulse summation process by adding the transmit fields obtained by exciting the annular transducer with pulse **103** and **104**, respectively. Tissue scattering and back-propagation of the scattered pulses are assumed to be linear processes. Performing pulse inversion on the obtained transmit fields thus give a good indication on how the harmonic pulse inversion process will affect the received tissue signals. **FIG.5** displays the spectrum of the resulting pulse summation signal at 6 cm on the symmetry axis. As expected from Eq.5, the fundamental component (**371**) is increased by around 6 dB relative to **FIG.4** while the linear transmitted second harmonic band is canceled and only a nonlinear component (**372**) remains. The third

harmonic band (**373**) is in the pulse summation process significantly reduced while the fourth harmonic band (**374**) shows an expected increase relative to **FIG.4**.

[0054] Performing a pulse subtraction of the two transmit fields obtained from pulse **103** and **104** we obtain the spectrum depicted in **FIG.6** at 6 cm on the symmetry axis. The linear fundamental band is now canceled and only a nonlinear component (**381**) can be seen. The linear second harmonic band (**382**) and nonlinear third harmonic band (**383**) are both increased by approximately 6 dB while the fourth harmonic band (**384**) is heavily suppressed relative to **FIG.4**. These results are in good agreement with Eq.6.

[0055] By removing the second harmonic band from the pulses in **FIG.2** they will all be identical. The transmit field from such a conventional single frequency band pulse is calculated. At 6 cm on the symmetry axis the spectrum of the transmit field is as shown in where a strong linear fundamental band (**391**) and a weak first order nonlinear band (**392**) are seen.

[0056] The transmit field from such a single frequency band pulse is used to drive a contrast bubble with resonance frequency around 3 MHz. The spectrum of the scattered bubble signal when applying the resulting transmit field at 6 cm on the symmetry axis as drive pulse is displayed in **FIG.8**. There is a strong scattered linear component (**301**) and first order nonlinear second harmonic component (**302**). Higher order nonlinear scattered components, third (**303**) and especially fourth (**304**) harmonic components, are weak.

[0057] Driving the same bubble with the transmit fields obtained from the dual frequency band pulses (**104** and **103**) we obtain the scattered spectra displayed in **FIG.9** and **FIG.10** at 6 cm on the symmetry axis. Due to the linear transmitted second harmonic component, the scattered second harmonic from the bubble (**312** and **322**) is increased. The scattered third (**313** and **323**) and fourth (**314** and **324**) harmonic bands are now mainly first order nonlinear terms and significantly increased relative to the situation applying a single frequency band pulse in **FIG.8**. Also important, we notice that there is a difference in scattered fundamental bubble signal (compare **311** and **321**) and scattered fourth harmonic bubble signal (compare **314** and **324**) applying the two pulses **104** and **103** with inverted polarity on the transmitted second harmonic band.

[0058] Performing pulse summation on the two scattered bubble signals driven by the dual frequency band transmit fields at 6 cm we obtain the spectrum depicted in **FIG.11**. Most important here is that the resulting third harmonic component (**343**), although somewhat reduced relative to **313** and **323**, is increased relative to **303**.

[0059] We may also do a pulse subtraction of the two scattered bubble signals driven by the dual frequency band transmit fields at 6 cm and the resulting spectrum is shown in **FIG.12**. When performing pulse subtraction we are especially interested in the resulting fundamental and fourth harmonic bands from the contrast bubble. Energy at these bands were in **FIG.6** seen to be very low for tissue (**381** and **384**). The pulse subtraction bubble signal, however, has a strong nonlinear fundamental component (**331**) only reduced by a few decibels compared to **311** in **FIG.9**. Transmitting dual frequency band pulses and doing pulse inversion on the transmitted second harmonic

band hence appears to be a very good alternative to contrast amplitude modulation technique with nonlinear fundamental imaging. The resulting fourth harmonic contrast component (334) is also very strong and can be the basis for image reconstruction.

[0060] FIG.13 displays the transmit pulse in the time domain at 10 cm on the symmetry axis resulting from driving the annular transducer with pulse 102 while FIG.14 displays the transmit pulse at the same location obtained with pulse 101. We notice the asymmetry with respect to positive and negative pressure amplitude when using the two excitation pulses with inverted polarity on the transmitted second harmonic band.

[0061] In FIG.15 the spectrum of pulse 105 is shown. In addition to the two strong linear components (461 and 462) a third harmonic band (463) and a fourth harmonic band (464) are present.

[0062] In the same way as was done at 6 cm we now perform pulse summation and pulse subtraction of the two transmit fields obtained from pulse 101 and 102 and the resulting spectra are shown in FIG.16 and FIG.17. As previously, when doing pulse summation we heavily suppress the second (472) and third (473) harmonic tissue components while the fundamental (481) and fourth (484) harmonic tissue components are suppressed when doing pulse subtraction.

[0063] A contrast bubble with resonance frequency around 3 MHz is then driven by the calculated transmit field at 10 cm on the symmetry axis from the fundamental band only of pulse 102. The spectrum of the resulting scattered bubble signal is depicted in FIG.18 and the bubble response is seen to be rather linear when driven by this low intensity single frequency band pulse.

[0064] The bubble is then driven by the calculated transmit field at 10 cm on the symmetry axis from pulse **102**. The spectrum of the resulting scattered bubble signal is depicted in **FIG.19**. Due to strong nonlinear scattering from the bubble, the third (**413**) and fourth (**414**) harmonic components are very high compared to **403** and **404** obtained using a single frequency band pulse.

[0065] In **FIG.20** the spectrum of the resulting pulse subtraction signal at 10 cm on the symmetry axis is seen for the situation when pulse **101** and **102** are used to drive the annular transducer. Again, we see a strong nonlinear fundamental band (**431**) and a strong fourth harmonic band (**434**) which can be used for image reconstruction of the contrast bubble since these components are heavily suppressed for tissue (**481** and **484**).

[0066] The new contrast specific imaging method presented is capable of significantly increasing the first order nonlinear signal scattered from contrast agents without increasing the resulting first order nonlinear signal scattered from tissue. This new method will thus give rise to detection of contrast agents in the presence of tissue with better sensitivity (CNR) and specificity (CTR).

[0067] Thus, while there have shown and described and pointed out fundamental novel features of the invention as applied to a preferred embodiment thereof, it will be understood that various omissions and substitutions and changes in the form and details of the devices illustrated, and in their operation, may be made by those skilled in the art without departing from the spirit of the invention. For example, it is expressly intended that all combinations of those elements and/or method steps which perform

substantially the same function in substantially the same way to achieve the same results are within the scope of the invention. Moreover, it should be recognized that structures and/or elements and/or method steps shown and/or described in connection with any disclosed form or embodiment of the invention may be incorporated in any other disclosed or described or suggested form or embodiment as a general matter of design choice. It is the intention, therefore, to be limited only as indicated by the scope of the claims appended hereto.